## Distortion Measurement Control Unit

## FEATURES:

- Swept two-tone generator and analyzer control for harmonic, differencefrequency and intermodulation distortion measurements
■ Frequency range 2 Hz to 200 kHz
- Typical distortion less than 0,01\%
- Amplitude linearity better than $\pm 0,2 \mathrm{~dB}$
- Automatic tuning of Heterodyne Analyzer Type 2010
- Automatic tracking on individual distortion components up to fifth order
- Automatic sweep with Level or X-Y Recorder
- Low frequency signal continuously adjustable from 20 Hz to 2 kHz in intermodulation mode
- Frequency difference continuously adjustable from 20 Hz to 2 kHz in difference-frequency mode
- Output voltages up to 10 V
- Output impedance of $600 \Omega$ or $5 \Omega$
- Easy to operate



## USES:

- Harmonic distortion measurements and analyses to DIN 45403 and IEC 268-3
- Difference-frequency distortion measurements and analyses to DIN 45403, IEC 268-3 and CCIF
■ Intermodulation distortion measurements and analyses to DIN 45403 , IEC 268-3 and SMPTE

The 1902 Distortion Measurement Control Unit is an advanced and accurate instrument designed to automatically control the wellknown Heterodyne Analyzer Type 2010 to provide swept measurement of non-linear distortion in amplifiers, loudspeakers, hearing aids, tape recorders, microphones, hydrophones etc.

The swept distortion measurements, introduced by the 1902/2010 combination, give more information and are easier to perform than the normally used
method of measuring distortion at several single frequencies, a method which is very tedious and may give results that are not truly representative.

The 1902/2010 measures harmonic distortion, difference-frequency distortion and intermodulation distortion all to DIN 45403 and IEC 2683 standards. Difference-frequency distortion and intermodulation distortion may also be measured according to the CCIF and SMPTE methods, respectively. Further with the addition of a Time Delay Spectrometry Unit Type 5842, free field measurments in ordinary environments may be carried out using a 1902 and 2010.

The 1902 provides tuning signals for the 2010 and generates the necessary test signals for swept measurement of distortion components up to fifth order, in the frequency range 2 Hz to 20 kHz . Distortion components down to typically -80 dB can be measured. Together with the Level Recorder Type 2307 or X-Y Recorder Type 2308 automatic analysis of distortion can be performed and documented on preprinted frequency-calibrated paper.

## Principle of Operation

Fig. 1 shows the principle of operation of the 1902 together with the 2010.

## Type 2010

The 2010 is a frequency selective measuring amplifier and a beat frequency oscillator, both normally interlocked to operate at the same frequency. It covers the frequency range from 2 Hz to 200 kHz and has six analysis bandwidths ranging from $3,16 \mathrm{~Hz}$ to 1000 Hz . For further information on Type 2010 see separate product data sheet.

## Type 1902

The 1902 is a two-tone generator which provides the necessary test signals for the measuring object, and a frequency synthesizer, providing a control signal to tune the analyzer section of the 2010 to the frequency of the desired distortion component.


Fig.1. Interconnection of Type 1902 and Type 2010

## 1902/2010 Combination

When the 1902 is connected to the 2010 (Fig.1), the interlock between the analyzer and oscillator sections of the 2010 is automatically released. This means that the oscillator section of the 2010 together with the two-tone generator of the 1902 can be swept independ-
ently of the analyzer section of the 2010, which can now be tuned to the desired distortion component by the frequency synthesizer of the 1902. The three cables (AO 0064) required for connection of the 2010 to the 1902 are supplied with the 1902.

## Description

The 1902 is equipped with three push-button controlled mode switches, "Harmonic", "Differencefrequency" and "Intermodulation", for selection of the distortion measuring mode. A five-position DISTORTION ORDER switch together with two push-button switches, " + " and "-", select the distortion component to be tracked by the 2010. A frequency calibrated dial is used for setting frequency differences between 20 Hz and 2 kHz when measuring difference-frequency distortion and for setting the lower test frequency when measuring intermodulation distortion.

As described above, the 1902 consists of a two-tone generator and a frequency synthesizer. In the following text a short description of the operation of the 1902 is given.

The clock frequency used in the 1902 is the $1,2 \mathrm{MHz}$ "Fixed Frequency" from the crystal-controlled


Fig.2. Simplified block diagram of the 1902 in the "Harmonic" mode
oscillator of the 2010, thereby ensuring perfect synchronization between the two instruments.

In Figs.2, 3 and 4, simplified block diagrams of the 1902 in the different modes of operation are shown. Fig. 5 shows the relative position of the frequencies obtained
from the 1902 in the different modes of operation and the corresponding analysis frequencies.

## Two-Tone Generator

The generator consists basically of a voltage controlled oscillator (VCO), two modulators, an output amplifier and an attenuator.

In the "Harmonic" mode the $1,2 \mathrm{MHz}$ "Fixed Frequency" and the 1,2 to 1 MHz "Variable Frequency" from the 2010 are fed to one of the modulators, mixed and then filtered in a 250 kHz low-pass filter (see Fig.2). The resulting signal ( $\mathrm{f}_{2}$ ) will have the same frequency as the signal from the BFO of the 2010. This frequency is indicated on the frequency counter display of the 2010. From the modulator, the signal is fed via the GENERATOR STOP switch to the output amplifier and the OUTPUT sockets.

The signal $\left(f_{2}\right)$ is used in all modes of the 1902 , and in the "Dif-ference-frequency" and "Intermodulation" modes, where two test tones are generated, it will always be the higher frequency of the two tones. See also Fig. 5.

In the "Difference-frequency" mode a second tone, which follows the frequency of $f_{2}$ at a preset frequency difference below $f_{2}$, is added. The frequency difference ( $f_{o}$ ) is set by means of the front panel frequency control potentiometer, which controls a VCO operating at $1,2 \mathrm{MHz} \pm f_{0}$ (see Fig.3). This frequency is mixed with the "Variable Frequency" from the 2010 $\left(1,2 \mathrm{MHz}-\mathrm{f}_{2}\right)$ in a modulator and filtered in a 250 kHz low-pass filter leaving the desired frequency component $f_{1}=f_{2}-f_{0}$. See Fig.5. $f_{o}$ is adjustable in the frequency range 20 Hz to 2 kHz . The two signals, $f_{1}$ and $f_{2}$, are then summed in the output amplifier to have equal amplitudes and an output voltage whose RMS value is the same as that of the single tone $\left(f_{2}\right)$ in the "Harmonic" mode.

In the "Intermodulation" mode, a fixed low frequency tone ( $f_{1}$ ) is used in addition to the sweeping tone ( $\mathrm{f}_{2}$ ). The frequency of this ( $\mathrm{f}_{1}$ ) tone can be set in the frequency range 20 Hz to 2 kHz by means of the front panel frequency control potentiometer. This tone $\left(f_{1}\right)$ is obtained by mixing the $1,2 \mathrm{MHz} \pm f_{o}$ from the VCO with the $1,2 \mathrm{MHz}$ "Fixed Frequency" in a modulator and filtering in a 250 kHz low-pass filter leaving $f_{0}\left(=f_{1}\right)$. See Fig.4. $f_{1}$ and $f_{2}$ are then summed in the output amplifier, so that the amplitude of $f_{1}$ is four times the amplitude of $\mathrm{f}_{2}$ ( 12 dB higher). See Fig. 5.


Fig.3. Simplified block diagram of the 1902 in the "Difference-frequency" mode


Fig.4. Simplified block diagram of the 1902 in the "Intermodulation" mode

The test signal which is available at the standard B \& K coaxial OUTPUT socket of the 1902, can be varied continuously from 0 to 10 V using the OUTPUT VOLTAGE potentiometer or in 10 dB steps from $100 \mu \mathrm{~V}$ to 10 V using the ATTENUATOR. The amplitude linearity of both frequencies is better than $\pm 0,2 \mathrm{~dB}$ over the entire 2 Hz to 200 kHz frequency range. The output Impedance is either $600 \Omega$ or $5 \Omega$, depending upon the setting of the ATTENUATOR. The test signal is also available at the coaxial BNC OUTPUT socket on the rear of the instrument (Fig.6). An ADJUST potentiometer on the rear panel is provided for adjusting the amplitude of $f_{2}$. The adjustment range is $\pm 1 \mathrm{~dB}$.

Two push-button switches, GENERATOR STOP, are provided to switch off one or both of the test frequencies when setting up and adjusting the test object.

## Frequency Synthesizer

The synthesizer which generates the control signal necessary to tune the analyzer section of the 2010 to any desired distortion component up to the fifth order in the frequency range 2 Hz to 200 kHz , consists of two phase-locked loops (PLL). The input frequencies to the synthesizer are the "Fixed Frequency" ( $1,2 \mathrm{MHz}$ ) and the "Variable Frequency" ( 1,2 to $1,0 \mathrm{MHz}$ ) from the 2010. The BNC input sockets for these signals are situated on
the rear of the 1902 together with the BNC output socket for the control signal, "External Variable Frequency", for the 2010. See Fig. 6.

In the "Harmonic" mode, the input to the first PLL is the $1,2 \mathrm{MHz}$ "Fixed Frequency". See Fig.2. The reference signal for the loop, which is 60 kHz , is derived from the $1,2 \mathrm{MHz}$ "Fixed Frequency" in the fixed frequency converter. The reference signal is multiplied by the distortion order number $n$ which is selected with the DISTORTION ORDER switch. Thus the output of the PLL is $1,2 \mathrm{MHz}+\mathrm{n} \times 60 \mathrm{kHz}$. This signal is fed to the second PLL where the 60 kHz component is substituted by $\mathrm{f}_{2}$, because the reference frequency in this loop is $60 \mathrm{kHz}+\mathrm{f}_{2}$. This gives an output frequency of $1,2 \mathrm{MHz}-n \times f_{2}$ which is the required signal for tuning the analyzer section of the 2010 to the $n^{\text {th }}$ harmonic of $f_{2}$. See Fig. 5.

The use of the 60 kHz reference frequency in the PLLs has two advantages: It permits simple frequency division to be employed for selection of the distortion order number and it gives the PLLs a fast response allowing the analyzer to track more rapidly than if the PLLs operated directly on the low frequency signal.

In the even order "Difference-frequency" modes ( $\mathrm{n}=2$ and 4), the operation of the first PLL is identical to the operation in the "Harmonic" mode, thus giving an output frequency $1,2 \mathrm{MHz}+\mathrm{n} \times 60 \mathrm{kHz}$. However, the second PLL now uses a reference signal, which is $60 \mathrm{kHz}+$ $f_{0}$, where $f_{o}$ is the frequency difference set with the frequency control potentiometer. The PLL therefore substitutes the 60 kHz component with $f_{0}$, giving an output frequency of $1,2 \mathrm{MHz}-n \times f_{o}$. Thus with $n=$ 1 , the 2010 will be tuned to the "2-" distortion order component ( $\mathrm{f}_{2}-\mathrm{f}_{1}=\mathrm{f}_{\mathrm{o}}$ ) and with $\mathrm{n}=2$, to the " $4-$ " component, that is the frequency difference and its second harmonic, respectively. See Figs. 3 and 5.

In the odd order "Difference-frequency" modes ( $\mathrm{n}=1,3$ and 5 ) the input to the first PLL is $1,2 \mathrm{MHz}$ $f_{0}$, which means that the output sig-


Fig.5. Relative position of analysis frequencies of 2010, and test signal frequencies of 1902 in the three different modes of operation

nal will be $1,2 \mathrm{MHz}-\mathrm{f}_{2}+\mathrm{n} \times$ 60 kHz . Again, the second PLL replaces the 60 kHz component with $f_{o}$. Now, depending on whether the reference signal is $60 \mathrm{kHz}+\mathrm{f}_{\mathrm{o}}$ or 60 kHz - $\mathrm{f}_{\mathrm{o}}$, the " + " or "-" distortion order component will be selected. The resulting analyzer control signal will therefore be $1,2 \mathrm{MHz}$ $-f_{2} \pm n \times f_{0}$. The reference signal is chosen with the " + " and "-" push-button switches. It should be noted that in this mode the frequency dividers in the PLLs do not divide by the actual distortion order number. For example, the " $3+$ " component lies $1 \times f_{0}$ above $f_{2}$, hence $n$ must be one. Likewise for the " $5+$ " and the " 3 -" components, $n$ must be 2 ; and for the " 5 -" component the dividers must divide by 3. See also Fig. 5.

The operation of the frequency synthesizer in the "Intermodulation" mode (Fig.4) is virtually identical to the operation in the odd order "Difference-frequency" mode, the only difference being that in the "Intermodulation" mode, the frequency dividers divide by the actual distortion order number $n-1$.

## Distortion

The distortion of the $1902 / 2010$ combination itself is very low. In the range from 100 Hz to 100 kHz the distortion is less than $0,02 \%$ and less than $0,03 \%$ in the range 15 Hz to 200 kHz , measured on any distortion component in any mode. Second order and third order distortion is typically less than $0,01 \%$ and fourth and fifth order less than 0,004\%. However, in the "Intermodulation" mode these figures may be

Diagram indicating the relative position of the analysis frequencies of the 2010 and the test signal frequencies of the 1902 in the different modes of operation

-position rotary-switch for selection of the order of the distortion component to be measured


Frequency calibrated dial for setting the frequency difference between the test frequencies in the "Difference - frequency" mode or setting the lower test frequency in the "Intermodulation" mode

ATTENUATOR variable in 10 dB steps for selection of output voltages between $0,1 \mathrm{mV}$ and 10 V . The output voltage is continuously variable with the OUTPUT VOLTAGE potentiometer within each step. The source impedance is $600 \Omega$. In the $10 \mathrm{~V} / 5 \Omega$-position the output voltage can be varied between 0 and 10 V and the source impedance is $5 \Omega$
OUTPUT VOLTAGE potentiometer for continuous variation of the voltage, either within each step of the ATTENUATOR ( $600 \Omega$ positions) or from 0 to 10 V ( $5 \Omega$ position)

improved by a factor of about three by inserting a high-pass filter between the output of the test object and the input of the analyzer as shown in Fig.7, to filter out the test frequency $f_{1}$.

The $1902 / 2010$ combination is self-checking, hence the output from the 1902 can be connected directly to the input of the 2010 in order to measure the distortion residual of the system in any mode.

## General

The 1902 is fully compatible with all Heterodyne Analyzers Type 2010 currently being delivered. However, for some earlier models of the 2010, modifications may be necessary. For 2010 s with serial numbers up to 401819 , an addi-
tional B \& K socket (EXTERNAL VARIABLE FREQUENCY 1,2 to $1,0 \mathrm{MHz}$ ) must be added to the rear panel to permit external control of the analyzer section. In addition, all
instruments up to serial number 476289 require a modification of the COUNTING TIME switch in order to be able to read the frequency to which the analyzer is tuned.

## Examples of Use

The great flexibility and versatility of the 1902/2010 combination allows detailed analysis of distortion to be carried out where this has previously been very difficult or even impossible.

The $1902 / 2010$ combination is mainly intended for measurements on Hi -Fi-sound reproduction and recording equipment such as microphones, loudspeakers, amplifiers, tape recorders, and telecommunication equipment, and transmission lines but it can also be employed in measurements on, for instance, pick-ups, hydrophones and projectors.

In the following section, a few examples of typical measuring setups, showing the possibilities of the system are given.

Fig. 8 shows a set-up which can be utilized for measurmement and analysis of harmonic, difference frequency or intermodulation distortion analyses on various types of equipment. By adding a Level Recorder Type 2307 or X-Y Recorder Type 2308 , the 2010 can be swept automatically and the measurement or analysis can be graphically presented on frequency calibrated paper.

Fig. 9 shows an analysis of the 3rd order ( - ) difference-frequency distortion of a $\mathrm{Hi}-\mathrm{Fi}$ tape recorder recorded by means of the set-up shown in Fig. 8.


Fig.7. Extending the dynamic range of the $1902 / 2010$ combination in the "Intermodulation" mode by means of a simple, high pass filter


Fig.8. Set-up for analysis of distortion on a tape recorder


Fig.9. Difference-frequency analysis recorded with the set-up in Fig. 8

In the set-up in Fig.10, the 1902/2010 are employed in measuring and recording the distortion characteristics of a loudspeaker. Efficient loudspeakers can be driven directly by the 1902 , while less effi-
cient loudspeakers require a power amplifier. Due to small dimensions and wide frequency range, a $1 / 2^{\prime \prime}$ Condenser Microphone, such as Type 4133, is preferred on the receiving side of the set-up.

The 1902 may also be employed in microphone measurements. Fig. 11 shows a set-up which will be very suitable for measurement of the intermodulation and differencefrequency distortion characteristics of microphones. Two loudspeakers are used, one for each test frequency, in order to eliminate the difference frequency and intermodulation distortion of the loudspeaker itself. The test frequency $f_{2}$ is obtained directly from the 2010, while the $f_{1}$ signal is supplied from the output of the 1902 , with the $f_{2}$ signal switched off by means of the GENERATOR STOP switch.

For free field measurements on loudspeakers and other electroacoustic equipment in ordinary, nonanechoic environments the instrument setup shown in Fig. 12 can be employed. This makes use of the Time Delay Spectrometry Unit Type 5842 for control of the 1902/2010 and together with a Phase Meter Type 2971 enables fast, time selective magnitude and phase response measurements to be made. Moreover, with the addition of a Type 2033 Narrow Band Spectrum analyzer, the magnitude versus time response may be obtained.

An important virtue of the Time Delay Spectrometry as performed by Type 5842 is its capability of rejecting noise and reflections. In addition it takes only a few seconds to complete a measurement plus provide an almost simultaneous graphical representation of the measured free


Fig.10. Set-up for recording the distortion characteristics of a loudspeaker


Fig.11. Set-up for recording intermodulation and difference-frequency distortion analyses of a microphone
field response on an oscilloscope. Alternatively where hard copy, plot is required, an X-Y Recorder such as Type 2308 can be included in the measurement setup.

For further details on this and other applications of the Time Delay Spectrometry Unit, please ask for the separate Product Data for Type 5842.


Fig. 12. Setup including the Time Delay Spectrometry Control Unit Type 5842 for free field loudspeaker measurements in ordinary environments

Input from 2010 (BNC
Fixed Frequency: $1,2 \mathrm{MHz}$ (clock frequency)
Variable Frequency: $1,2 \mathrm{MHz}$ to $1,0 \mathrm{MHz}$

Test Signals:
Harmonic Mode: Single tone ( $\mathrm{f}_{2}$ ) swept from 2 Hz to 200 kHz
Difference-frequency Mode: Two tones ( $f_{1}$ and $f_{2}$ ) with a fixed frequency difference adjustable from 20 Hz to 2 kHz , swept from 2 Hz to 200 kHz . The tones are of equal amplitude
Intermodulation Mode: Two tones, one fixed ( $f_{1}$ ) and one swept ( $f_{2}$ ) from 2 Hz to $200 \mathrm{kHz} . f_{1}$ is adjustable from 20 Hz to 2 kHz and is 12 dB higher than $\mathrm{f}_{2}$

## Sweep Characteristics:

Linear or logarithmic (see Product Data for Type 2010)

Amplitude Linearity of $\mathrm{f}_{1}$ and $\mathrm{f}_{\mathbf{2}}$ $\pm 0,2 \mathrm{~dB}$ from 2 Hz to 200 kHz

## Noise and Hum:

$<-70 \mathrm{~dB}$ ( 2 Hz to 200 kHz )
Attenuator Output:
Output Voltage: $100 \mu \mathrm{~V}$ to 10 V , variable in steps of 10 dB and continuously variable within each step
Accuracy of Steps: $\pm 0,1 \mathrm{~dB}$ re 10 V position
Output Impedance: $600 \Omega$ (unbalanced) in all attenuator positions

## Direct Output

Output Voltage: 0 to 10 V continuously variable
Maximum Output Current: 40 mA peak (short circuit protected)
Maximum Output Power: 500 mW into $200 \Omega$
Output Impedance: $5 \Omega$ (unbalanced) DC Offset: $< \pm 50 \mathrm{mV}$

Frequency Dial:
Intermodulation Mode: Sets $f_{1}$ from 20 Hz to 2 kHz
Difference-frequency Mode: Sets $\mathrm{f}_{2}$ $\mathrm{f}_{1}$ from 20 Hz to 2 kHz
Accuracy: $\pm 4 \%$

## FREQUENCY SYNTHESIZER

Input from 2010 (BNC)
Fixed Frequency: $1,2 \mathrm{MHz}$ (clock frequency)
Variable Frequency: 1.2 MHz to $1,0 \mathrm{MHz}$

## Output to 2010

External Variable Frequency: $1,2 \mathrm{MHz}$ to $1,0 \mathrm{MHz}$ to tune the 2010 to the selected distortion component in the frequency range 2 Hz to 200 kHz . See the table

## 1902/2010 SYSTEM

## Measuring Modes:

Harmonic, difference-frequency and intermodulation distortion up to 5 th order. All distortion components are measured individually. See the table

Distortion of 1902/2010 System:
$<0,02 \%$ from 100 Hz to 100 kHz
< 0,03\% from 15 Hz to 200 kHz
(any component in any mode)

Typical Distortion of the System:
2nd or 3rd Order Distortion: $<0,01 \%$
4th or 5th Order Distortion: < 0,004\%

Maximum Sweep Rate:
$5 \mathrm{~s} /$ decade while maintaining phase-lock (maximum paper speed of $10 \mathrm{~mm} / \mathrm{s}$ on Level Recorder Type 2307)

Analyzer Inputs and Filter characteristics:
See Product Data for Type 2010

## Temperature Range:

$10^{\circ}$ to $40^{\circ} \mathrm{C}\left(50^{\circ}\right.$ to $\left.140^{\circ} \mathrm{F}\right)$

Max. Humidity:
$90 \% \mathrm{RH}$ (non condensing) at $30^{\circ} \mathrm{C}$

Electromagnetic Compatibility:
Complies with Class B device of American FCC (Federal Communication Commission) Rules

## Power Supply:

$100,115,127,220,240 \mathrm{~V}(50$ to 60 Hz$)$
$A C \pm 10 \%$
Complies with IEC 348 safety class I

## Power Consumption:

Approximately 25 VA

| Mode Switch Position |  | Distortion Order Switch Position | Test Frequencies (1902) | Analysis Frequency (2010) |
| :---: | :---: | :---: | :---: | :---: |
| Harmonic |  | 1 | $\mathrm{f}_{2}$ | $\mathrm{f}_{2}$ |
|  |  | 2 |  | $2 \times 12$ |
|  |  | 3 |  | $3 \times 12$ |
|  |  | 4 |  | $4 \times \mathrm{f} 2$ |
|  |  | 5 |  | $5 \times \mathrm{f}_{2}$ |
| Difference frequency | + | 1 | $\mathrm{f}_{2}$ | $\mathrm{f}_{2}$ |
|  |  | 3 | $f_{2}$ and $f_{1}$ | $2 f_{2}-f_{1}$ |
|  |  | 5 |  | $3 f_{2}-2 f_{1}$ |
|  | - | 2 |  | $\mathrm{f}_{2}-\mathrm{f}_{1}$ |
|  |  | 3 | Amplitude ratio:$f_{1}: f_{2}=1: 1$ | $2 f_{1}-f_{2}$ |
|  |  | 4 |  | $2 f_{2}-2 f_{1}$ |
|  |  | 5 |  | $3 \mathrm{f}_{1}-2 \mathrm{f}_{2}$ |
| Intermodulation | + | 1 | $\mathrm{f}_{2}$ | $\mathrm{f}_{2}$ |
|  |  | 2 | $\mathrm{f}_{2}$ and $\mathrm{f}_{1}$ | $\mathrm{f}_{2}+\mathrm{f}_{1}$ |
|  |  | 3 |  | $\mathrm{f}_{2}+2 \mathrm{f}_{1}$ |
|  |  | 4 |  | $\mathrm{f}_{2}+3 \mathrm{f}_{1}$ |
|  |  | 5 |  | $\mathrm{f}_{2}+4 \mathrm{f}_{1}$ |
|  | - | 2 |  | $\mathrm{f}_{2}-\mathrm{f}_{1}$ |
|  |  | 3 | Amplitude ratio:$f_{2}: f_{1}=1: 4$ | $\mathrm{f}_{2}-2 \mathrm{f}_{1}$ |
|  |  | 4 |  | $\mathrm{f}_{2}-3 \mathrm{f}_{1}$ |
|  |  | 5 |  | $\mathrm{f}_{2}-4 \mathrm{f}_{1}$ |

## Cabinet:

Supplied as model A (light-weight metal cabinet), B (model A in mahogany cabinet) or C (as A but with flanges for standard $19^{\prime \prime}$ racks)

Dimensions (A-Cabinet):
Height: $133 \mathrm{~mm}(5,2 \mathrm{in})$
Width: 380 mm ( 15 in )
Depth: 200 mm ( $7,9 \mathrm{in}$ )

Weight:

## $5,8 \mathrm{~kg}(13 \mathrm{lb})$

## Accessories Included

3 Cables AO 0127
B \& K Coaxial Plug JP 0101
BNC Plug JP 0035 Banana Plugs JB 0002 Power Cable AN 0010 315 mA Fuse VF 0042
200 mA Fuse VF 0012

